

Stress Analysis And Design Optimization Of Crankpin

S. M. Sorte, S. M. Sheikh

Abstract— the stress analysis and design optimization of a single cylinder crankpin of TVS Scooty Pep crankshaft assembly are discussed using stress analysis in this paper. Three-dimension models of crankshaft and crankpin forces were created using Pro/ENGINEER software and software ANSYS was used to analyze the stress status on the crankpin. The maximum deformation, maximum stress point and dangerous areas are found by the stress analysis. The relationship between the crank rotation and load acting on crank pin would provide a valuable theoretical foundation for the optimization and improvement of crankpin and engine design. [2]

Keywords— stress analysis; crankshaft; crankpin

I. INTRODUCTION

Crankshaft of Internal Combustion Engine is a well known phenomenon. The problem of their premature failure has attracted several investigators for over a century. The extensive studies have been made to identify the cause of failure and several have been listed.

Forces acting on the crankpin are complex in nature. The piston and the connecting rod transmit gas pressure from the cylinder to the crankpin. It also exerts forces on the crankpin, which is time varying. In this project one crank model of TVS Scooty pep will used to calculate the effect of stresses.

Crankshaft consists of the parts which revolve in the main bearings, the crankpin to which the big ends of the connecting rod is connected, the crank arms or webs (also called cheeks) which connect the crankpins and the shaft parts. The crankpin is like a build in beam with a distributed load along its length that varies with crank position. [1]

Reasons for Failure of crankshaft assembly and crankpin may be –

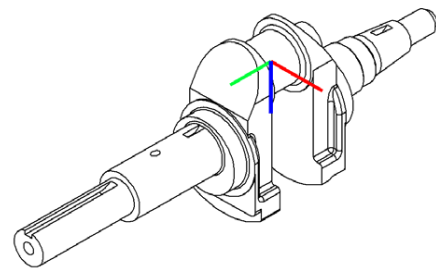
- A) Shaft misalignment
- B) Vibration cause by bearings application
- C) Incorrect geometry(stress concentration)
- D) Improper lubrication
- E) High engine temperature
- F) Overloading
- G) Crankpin material & its chemical composition
- H) Pressure acting on piston

II. OVERVIEW

In the process of converting the linear reciprocating motion of the pistons into a rotational output, the crankshaft undergoes both bending and torsion. [3]

As these forces are transmitted through the crankshaft, it becomes highly stressed, particularly so at the crankpin/web and the journal/web intersections of the cranked shaft.

As a consequence, fillet radii are used in these areas to reduce the stresses, but if the shaft is not carefully designed, these stresses can still reach unacceptably high levels with regard to material strength and fatigue life. [5]



Force acting on crankpin
Radial force, Tangential force, Inertia force STRESSES DUE TO FORCES ON CRANK PIN Bending stress and Shear stress

III. ENGINE SPECIFICATION

Table 1. Engine specification of TVS Pep

ENGINE SPECIFICATIONS		
1	CYLINDER BORE	51MM
2	STROKE	43MM
3	PISTON DISPLACEMENT	87.8CC
4	COMPRESSION RATIO	10.1:1
5	MAXIMUM POWER IN KW	3.68@6500RPM
6	MAXIMUM TORQUE IN NM	5.80@4000RPM
7	MAX. SPEED	60KM/HR
8	BEARING PRESSURE	7-12.5 N/MM ²



Fig.1 (20CrMo) High Precision Engine Crank Pin

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Fig.2 Crankshaft of TVS pep

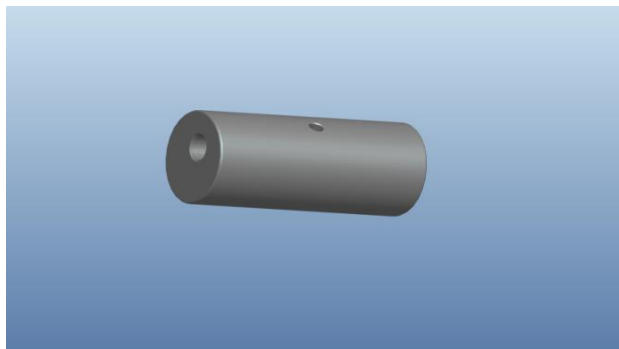


Fig.3 Model of crank pin

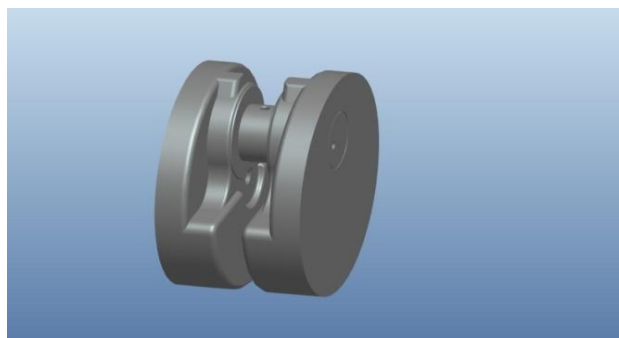


Fig.4 Model of crankshaft assembly

IV. DESIGN SPECIFICATION

Crankpin material –20CrMo
 (Chromium nickel Alloy steel)
 Crankpin diameter – 23mm
 Crankpin axial length – 40mm
 Crank web thickness – 15mm
 Crank web Height – 85mm
 Length of connecting rod – 90mm

Table 2.Crank Material and design Stresses

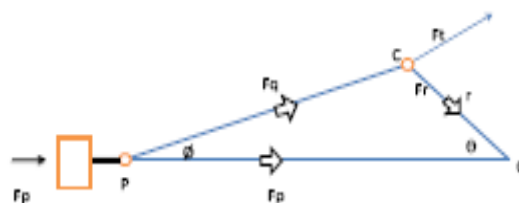
MATERIAL USED	ENDURANCE LIMIT (MPA)		ALLOWABLE SHEAR STRESS (MPA)	
	BENDING	SHEAR	BENDING	SHEAR
CHROME NICKEL	525	290	130 TO 175	72.5 TO 97
CARBON STEEL AND CAST STEEL	225	124	56 TO 75	31 TO 42
ALLOY CAST IRON	140	140	35 TO 47	35 TO 47

V. OBJECTIVE

Analyze the stresses acting on crank pin due to the gas force. Analyze the maximum deformation, maximum stress point and dangerous areas of failure. Optimize the design to reduce the rate of failure and improve the life of crank shaft and engine also if possible.

VI. METHODOLOGY

Let
 P = max. Pressure of gas
 D =Diameter of piston
 mR= mass of reciprocating parts
 ω = angular speed of crank
 Θ = angle of inclination of crank from top dead center
 \emptyset = angle of inclination of connecting rod with the line of stroke
 r= radius of crank
 l= length of connecting rod
 n= ratio of (l/r)
 dc= diameter of crank pin
 lc= length of crank pin
 FL = Force on piston due to gas pressure i.e. (p*A)



FI = Inertia force of reciprocating part
 i.e. (mR* ω^2 *r (cos Θ +cos2 Θ /n))
 Fp=net force on crank pin
 $F_L \pm F_I$
 Fc = force on connecting rod
 $F_c = F_p / \cos \emptyset$
 F_I = inertia force on crank pin
 $m * r * \omega^2$
 Pc = load on crank pin
 $dc * lc * pbc$
 F_T = tangential force on crank pin
 $F_Q \sin (\Theta + \emptyset)$
 F_R = radial force on crank pin
 $F_Q \cos (\Theta + \emptyset)$
 H_{T1} and H_{T2} =reaction at bearing due to F_T
 $F^T * b_1 / b$ and $F^T * b_2 / b$
 H_{R1} and H_{R2} = reaction at bearing due to FR
 $F_R * b_1 / b$ and $F_R * b_2 / b$
 Mc = max.bending moment on crank pin
 $H_{R1} * b_2$
 Tc = max.twisting moment on crank pin
 $H_{T1} * r$
 Te = equivalent twisting moment on crank pin
 $\sqrt{[(Mc^2) + (Tc^2)]}$
 τ = max. Shear stress on pin
 $Te / (\pi / 16) * dc^3$
 Let max. Bearing pressure (Pb) – 12.5 N/mm² So, load on crank pin
 $(F_L) = dc * lc * Pb = (23 * 40 * 12.5) = 11500N.$
 Max. Gas pressure on piston (P) =
 $(\pi / 4 * D^2) / (F_L) = 5.62 N/mm^2$



Net force acting on crank pin (Fp) = (F_L), neglecting inertia force.

Thrust on crank pin (Fq) = F / cosØ,

Where Ø = 28

F_q = 13024.5 N

VII. STRESS CALCULATION RESULT

Table 3. Tangential force and Radial force

SN	Ø	Θ	F _t (N) = F sin (Θ+Ø)	F _r (N) = F cos (Θ+Ø)
1	28	90	11.4*10	-6.1*10
2	0	180	0	-12.3*10
3	28	270	-11.4*10	6.1*10
4	0	360	0	12.3*10

Table 4. Bearing Reactions

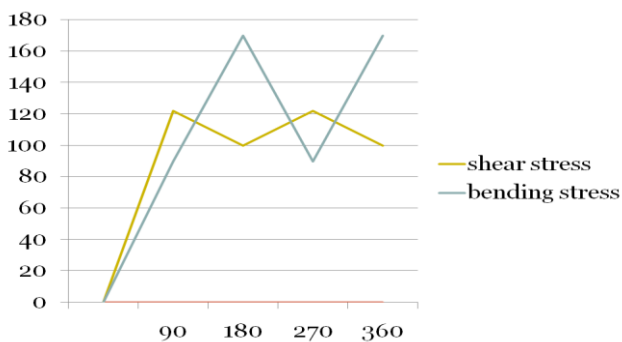
S N	Ø	Θ	HT1 = F _T * b / b ₁	HR1 = F _R * b / b ₁
1	28	90	5.7*10	-3.05*10
2	0	180	0	6.16*10
3	28	270	-5.7*10	3.05*10
4	0	360	0	6.16*10

Table 5. Bending Stress

S N	Ø	Θ	M _c = H _{RI} * b ₂	σ _b = M _c / [π/32 * d _c ³] N/mm ²
1	28	90	-106.7*10	90
2	0	180	215.6*10	180
3	28	270	106.7*10	90
4	0	360	-215.6*10	180

Table 6. Shear Stress

S N	Ø	Θ	τ = [Te / (π/16) * d _c ³] N/mm ²
1	28	90	267.3*10
2	0	180	215.6*10
3	28	270	267.3*10
4	0	360	215.6*10



Graph 1. Crank angle Vs Stresses

X- CRANK ANGLE, Y- STRESSES

VIII. CONCLUSION

Analytically it is to be concluded that the value of Max. shear stress is 112N/mm² and Max. Bending stress is 180 N/mm² which is more than the value of allowable stress value of material without taking any factor of safety. The relationship between the crank rotation and force acting on crank pin would provide a valuable theoretical foundation for the material selection and design optimization of crankpin and engine design.

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