

# Comparative Study of Design of Steel Structural Elements by using IS 800:2007, AISC 13<sup>th</sup> Edition and BS: 5950, 1:2000

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**Abstract-** *The task of the structural engineer is to design a structure which satisfies the needs of the client and the user. Specifically the structure should be safe, economical to build and maintain, and aesthetically pleasing. By considering the above needs of user this study gives the comparative design of structural element by using three different International Design Codes. Structural Elements such as tension member, compression member, flexural member, beam column, gusseted base, and beam column connection are designed for this comparative study. Same data is considered for the design of particular element and that element is designed by using Indian Standard (IS 800:2007), American Standard (AISC 13<sup>th</sup> Edition) and British Standard (BS 5950, 1:2000). The design methodology used in this study is same for all the codes but there are some differences in the constants or parameters depending on the code used. Finally the results are evaluated and compared in the tabular format.*

**Keywords**–IS 800:2007, AISC 13<sup>th</sup> edition, BS 5950 1:2000, LRF, and ASD.

## I. INTRODUCTION

In the present work, the detailed study of Design of structural element by using American Institute of Steel Construction and British Standard has been carried out with the comparison to the results by IS 800:2007 and submitted the comparative study of the same in the form of tables, which highlights the actual economy achieved by different codes of design for different structural sections. The observations made based on this study are very much necessary to the practicing structural engineers. The introduction of the paper should explain the nature of the problem, purpose, and the contribution of the paper.

The design of steel elements can be done by two methods:

### 1.1 Allowable Stress Design (Working Stress Method)

Working stress method of design based on the elastic theory in which material is assumed to be stressed well below its elastic limit under the design loads. The method, since relates safety to stress, defines factor of safety as the ratio of ultimate stress or yield stress to allowable or safe stress. This method is a well established method and that the method is simple in application and reliable

### 1.2 Load and Resistance Factor Design (Limit state Design)

The limit state method uses concept of fitness of the structure to perform its function satisfactorily during its service life span.

The condition or the state at which structure becomes unsafe is called the limit state and the philosophy based on this concept is called limit state philosophy of design. This method is more general in comparison to the working stress method. Several independent factors are used in the limit state design, each of which plays a particular role to ensure the reliability of the structure and the guarantee against the occurrence of a limit state

## 1.3 Design Codes

Structural design is a major activity of the profession of structural engineering. The designers can call on their creative spirit to design an infinite scope of outcomes but there are some severe restrictions on this freedom, namely economics and the demands posted by the requirements of the structural design standards, sometimes called codes or design specifications.

A standard code serves as a reference document with important guidance. The contents of the standard code generally cover details of design. These details include the basis and concept of design, specifications to be followed, design methods, safety factors, loading values and etc. In present days, many countries have published their own standard codes. These codes were a product of constant research and development, and past experiences of experts at respective fields. Meanwhile, countries or nations that do not publish their own standard codes will adopt a set of readily available code as the national reference. Some of them are Indian standard, American standard, British standard, Euro standard, Japan code, Canadian standard etc.

### 1.4 Objective

This study aimed to design all structural Steel elements as per IS 800:2007, AISC 13<sup>th</sup> manual and BS 5950-1:2000 guidelines and their comparison.

## II. SYSTEM DEVELOPMENT

There are various international codes available for the design of steel structures. Developments are still going on to achieve the great economy by using different methods as well as by using different codes of practice. In this chapter various designs are presented using three codes that is IS code, AISC code and BS code with step by step procedure.

This study gives the method of design of structural elements by different codes and comparison of results. Here design example of tension member will describes the methodology by IS method, BS method and AISC method.

### 2.1 Design Example

Design a tension member for unequal angle section of length 3 m, load on the member is

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225 kN; diameter of bolt is 20mm.

### 2.1.1 Solution by IS Method

$$\text{Yield strength of member} = \frac{A_g \cdot f_y}{\gamma_{mo}}$$

Where,

$$\text{Yield Stress} = F_y = 250 \text{ Mpa.} \quad [\text{Assumed}]$$

$$\text{Partial Safety Factor} = \gamma_{mo} = 1.1 \quad [\text{table no-5, IS: 800}]$$

$$\text{Therefore, } 225 \times 10^3 = A_g \times 250 / 1.1$$

$$\text{Gross area } A_g = 225 \times 10^3 \times 1.1 / 250 = 990 \text{ mm}^2$$

By using calculated gross area choose section from steel table having area slightly greater than the calculated.

Section chosen from steel table is

$$\text{ISA: } 100 \times 75 \times 8 \text{ mm.}$$

Sectional Properties of the same section from the steel table are as follows:

$$A_g = 13.36 \text{ cm}^2 = 1336 \text{ mm}^2$$

To calculate the strength of one bolt, thickness of gusset plate should be known hence, assume the thickness of gusset plate is 10 mm.

Strength of one bolt [IS : 800, Pg. No.- 75]

Strength of one bolt as per Standards is the minimum strength by shear strength or bearing strength of the bolt.

Shear strength [IS : 800, Pg. No.- 75]

Shear strength of bolt is

$$V_{dsb} = \frac{f_u (n_s A_{sb} + n_{sb} A_{sb})}{\sqrt{3} \gamma_{mb}}$$

Where, Ultimate yield strength =  $f_u = 410 \text{ Mpa}$

Number of shear planes with threads intercepting the shear plane =  $n_s = 0$

Number of shear planes without threads intercepting the shear planes =  $n_{sb} = 0.78$

$$\text{Nominal plain shank area of bolt} = A_{sb} = \pi / 4 \times (20)^2 = 314.15 \text{ mm}^2$$

Partial Safety Factor for bearing type  $\gamma_{mb} = 1.25$

[IS 800, table no- 5, page no -30]

Therefore, shear strength is,

$$V_{dsb} = \frac{410 \times (0 \times A_{sb} + 0.78 \times 314.15)}{\sqrt{3} \times 1.25} = 46.40 \text{ kN}$$

Bearing Strength [IS : 800, Pg. No.- 75]

Bearing strength of bolt is

$$V_{dps} = \frac{2.5 \times K_b \times d \times t \times f_u}{\gamma_{mb}}$$

$$\text{Constant} = K_b = \min \left( \frac{e}{3d_0}, \frac{p}{3d_0} - 0.25, \frac{f_u}{f_y}, 1 \right)$$

Here to calculate the constant  $K_b$  the values of end distance and pitch should be known therefore Assume, End distance (e) = 40 mm and Pitch (P) = 60 mm

Therefore,  $K_b = 0.66$

$$V_{dps} = \frac{2.5 \times 0.66 \times 20 \times 8 \times 410}{1.25} = 86.592 \text{ kN}$$

As per IS 800 the strength of bolt is the least value from bearing strength or shear strength, here minimum value is of shear strength, therefore

Strength of one bolt = min. from  $V_{dsb}$  and  $V_{dps}$

$$\text{Strength of one bolt} = 46.40 \text{ kN}$$

No of bolts can be calculated by knowing the total load applied on the member and the strength of one bolt and here both values are known therefore,

$$\text{No. of bolts} = \frac{\text{Total load}}{\text{strength of one bolt}} = \frac{225}{46.40} = 4.84 \sim 5 \text{ No.}$$

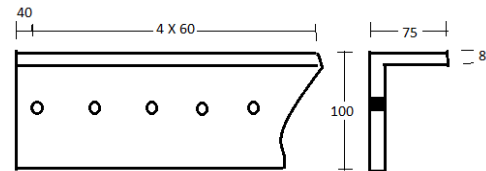


Fig.2.1 Design of Tension Member

Check for Design

Check for the design of tension member is taken as, the tensile strength of designed member should be greater than the load applied on the member, and the tensile strength nothing but the least value from strength due to yielding, strength due to rupture and strength due to block shear.

Strength against yielding

$$T_{dg} = \frac{A_g \cdot f_y}{\gamma_{mb}} = (1336 \times 250) / 1.1 = 303.63 \text{ kN} > 225 \text{ kN}$$

.....OK

Strength against rupture

$$T_{dn} = \frac{\alpha \cdot A_n \cdot f_u}{\gamma_{m1}}$$

Where,  $\alpha = 0.8$  because number of bolts are 5

[IS 800 : 2007, page no - 33]

Net area = total gross area – area of hole

$$A_n = 1336 - (22 \times 8) = 1160 \text{ mm}^2$$

$$T_{dn} = \frac{0.8 \times 1160 \times 410}{1.25} = 304.38 \text{ kN} > 225 \text{ kN} \quad \dots \text{OK}$$

Strength against block shearing [IS 800:2007, page no -33]

As per IS 800 :2007 strength of member due to block shear is calculated by two formulae and smaller one is supposed to be the final strength of member due to block shear.

$$A_{vg} = (40 + 60 \times 4) \times 8 = 2240 \text{ mm}^2$$

Where,

$A_{vg}$ ,  $A_{vn}$  = minimum gross and net area in shear along bolt line parallel to external force, respectively

$A_{tg}$ ,  $A_{tn}$  = minimum gross and net area in tension from the bolt hole to the toe of the angle, end bolt line, perpendicular to the line of force, respectively

$$A_{vn} = A_{vg} - (4.5 \times 22 \times 8) = 1448 \text{ mm}^2$$

$$A_{tg} = (100 - 40) \times 8 = 480 \text{ mm}^2$$

$$A_{tn} = A_{tg} - (0.5 \times 22 \times 8) = 392 \text{ mm}^2$$

$$T_{db1} = \frac{\text{Avg. } f_y}{\sqrt{3} \cdot Y_{mo}} + \frac{0.9 A_{tn} \cdot f_y}{Y_{m1}}$$

$$T_{db1} = \frac{2240 \times 250}{\sqrt{3} \times 1.1} + \frac{0.9 \times 392 \times 410}{1.25} = 409.642 \text{ kN}$$

$$T_{db2} = \frac{0.9 \times A_{vn} \times f_u}{\sqrt{3} \cdot Y_{m1}} + \frac{A_{tg} \cdot f_y}{Y_{mo}}$$

$$= \frac{0.9 \times 1448 \times 410}{\sqrt{3} \times 1.25} + \frac{480 \times 250}{1.1} = 355.879 \text{ kN}$$

Therefore, Strength against block shear = min. from  $T_{db1}$  &  $T_{db2}$   
= 355.879 kN > 225 kN.....OK

Use Angle section of size - 100×75×8 mm with 5nos. of bolts having 20mm dia. bolts.

All checks are satisfied hence the designed member is safe.

### 2.2.2 Solution by AISC Method

Here, assume the grade of steel is A36 therefore yield strength  $f_y = 36$  ksi and ultimate strength  $f_u = 58$  ksi.

As per AISC manual, strength =  $f_y \times A_g \times \phi$

[AISC; page no-1503; eq no- D2-1]

Where, strength is nothing but the total load applied on the member = 50.56

Yield strength =  $f_y = 36$  and Constant =  $\phi = 0.9$

Therefore,  $50.56 = 36 \times A_g \times 0.9$

$$A_g = 50.56 / (36 \times 0.9) = 1.56 \text{ in}^2$$

Hence, calculated gross area is  $1.56 \text{ in}^2$ , now choose an unequal angle section from AISC manual which has the same or slightly more area than calculated gross area.

$$L 4 \times 3 \times \frac{5}{16} \quad [\text{AISC; Table-5-2; page no-5-16}]$$

From the manual the gross area of the section chosen from table is  $20.9 \text{ in}^2$

By assuming thickness of gusset plate = 0.39 inch, the strength of bolt can be calculated, strength of one bolt is the least value from bearing strength or shear strength.

Bearing strength

$$\phi R_n = \phi \times 1.2 \times L_c \times t_a \times f_u [\text{AISC; eqn- J3-2a}]$$

Where, constant =  $\phi = 0.75$

Clear distance between edge of one hole to other hole

$$L_c = P - d_o = 2.36 - 0.79 = 1.57 \text{ inch}$$

$$\phi R_n = 0.75 \times 1.2 \times 1.57 \times 5/16 \times 58 = 25.61 \text{ kip}$$

$$\text{Shear strength } \phi R_n = \phi \times F_v \times A_b \times N_s$$

where, constant =  $\phi = 0.75$

Bolts ultimate shear stress =  $F_v = 58$  ksi

Nominal cross-sectional area of bolt =  $A_b = \pi/4 d^2 = 0.49 \text{ in}^2$

No of shear planes =  $N_s = 0.78$

$$\phi R_n = 0.75 \times 58 \times 0.49 \times 0.78 = 16.63 \text{ kip}$$

As per AISC, Strength of bolt is smaller of shear strength or bearing strength = 16.63 kip

No of bolts can be calculated by knowing the total load applied on the member and the strength of one bolt and here both values are known therefore,

$$\text{No. of bolts} = \frac{\text{Total load}}{\text{strength of one bolt}} = 50.56 / 16.63$$

$$= 3.04 \sim 3 \text{ Nos.}$$

Check for strength

Check for the design of tension member is taken as, the tensile strength of designed member should be greater than the load applied on the member, and the tensile strength nothing but the least value from strength due to yielding, strength due to rupture and strength due to block shear.

Strength against yielding

$$\phi R_n = \phi \times 0.6 \times A_v \times f_y \quad [\text{AISC; eqn J5-3}]$$

Where, constant =  $\phi = 0.9$

$$\text{Gross area} = A_v = h_a \times t_a = 118.11 \times 5/16 = 36.91 \text{ in}^2$$

Yield strength =  $F_y = 36$  ksi

$$\phi R_n = 0.9 \times 0.6 \times 36.91 \times 36 = 71.753 \text{ kip} > 50.56 \text{ kip}$$

....OK

Strength against rupture

$$\phi R_n = \phi \times 0.6 \times A_{vn} \times f_u \quad [\text{AISC; J4-1}]$$

Where, constant =  $\phi = 0.75$

$$\text{Net area} = A_{nv} = [h_a - n(d_h + \frac{1}{16})] t_a$$

$$= [118.11 - 3(0.87 + \frac{1}{16})] \frac{5}{16} = 36.04 \text{ in}^2$$

Ultimate strength =  $F_u = 58$  ksi

$$\phi R_n = 0.75 \times 0.6 \times 36.04 \times 58 = 940.64 \text{ kip} > 50.56 \text{ kip}$$

....OK

Strength against block shear [AISC; J4-5]

$$\phi R_n = \phi [0.6 \times f_u \times A_{gt}] \leq \phi [0.6 \times f_u \times A_{vn} + f_u \times A_{nt}]$$

Where,  $A_{gv}$ ,  $A_{nv}$  = minimum gross and net area in shear along bolt line parallel to external force, respectively

$$A_{gv} = 7.08 \times \frac{5}{16} = 2.21 \text{ in}^2$$

$$A_{nv} = A_{gv} - (2.5 \times 0.87 \times \frac{5}{16}) = 1.53 \text{ in}^2$$

$A_{gt}$ ,  $A_{nt}$  = minimum gross and net area in tension from the bolt hole to the toe of the angle, end bolt line, perpendicular to the line of force, respectively

$$A_{gt} = 2.43 \times \frac{5}{16} = 0.76 \text{ in}^2$$

$$A_{nt} = A_{gt} - (0.5 \times 0.87 \times \frac{5}{16}) = 0.62 \text{ in}^2$$

$$\phi R_n = 0.75 [(0.6 \times 58 \times 1.53) + (36 \times 0.76)] \leq 0.75 [(0.6 \times 58 \times 1.53) + (58 \times 0.62)]$$

$$= 60.45 \leq 66.90 = 60.45 \text{ kip} > 50.56 \text{ kip} \quad \text{.....OK}$$

Use angle section of size  $L 4 \times 3 \times \frac{5}{16}$  with 3 nos. of bolts having dia. 0.79 inch

All checks are satisfied hence the designed member is safe.

### 2.2.3 BS Method

$$\text{Yield strength of member} = \frac{A_g \cdot f_y}{\gamma_{mo}} = 225 \times 10^3 = \frac{A_g \times 250}{1}$$

Therefore gross area of the section is  $A_g = 900 \text{ mm}^2$

By using calculated gross area choose section from BS manual having area slightly greater than the calculated.

Section chosen from BS 5950 manual is

$$100 \times 75 \times 8 \text{ mm [BS EN; B-41;]}$$

Sectional Properties of the same section from the steel table are as follows:  $A_g = 1350 \text{ mm}^2$

To calculate the strength of one bolt, thickness of gusset plate should be known hence, assume the thickness of gusset plate is 10 mm.

Strength of one bolt

Strength of one bolt as per Standards is the minimum strength by shear strength or bearing strength of the bolt.

Shear strength  $P_s = p_s \cdot A_s$  [BS: 5950; 135; table-30]

$$\text{Where, } p_s = 160 \text{ and } A_s = \text{shear area} = \frac{\pi d^2}{4}$$

$$= (\pi 20^2)/4 = 314.16 \text{ mm}^2$$

$$P_s = 160 \times 314.16 = 50.26 \text{ kN}$$

Bearing Strength

$$P^{bb} = d \times t \times p^{bb} \quad [\text{BS : 5950; 136; table-31}]$$

Where,  $d = \text{dia. Of bolt} = 20 \text{ mm}$

ThickNess of section =  $t_p = 8 \text{ mm}$

$$\text{Bearing strength} = p^{bb} = 460$$

$$P^{bb} = 20 \times 8 \times 460 = 73.6 \text{ kN}$$

Strength of one bolt as per Standards is the minimum strength by shear strength or bearing strength of the bolt.

Therefore, Strength of bolt = 50.26 kN

No of bolts can be calculated by knowing the total load applied on the member and the strength of one bolt and here both values are known therefore,

$$\text{No. of bolts} = \frac{\text{Total load}}{\text{strength of one bolt}} = 225/50.26 = 4.45 \sim 5 \text{ nos.}$$

Check for strength

Check for the design of tension member is taken as, the tensile strength of designed member should be greater than the load applied on the member, and the tensile strength nothing but the least value from strength due to yielding, strength due to rupture and strength due to block shear.

Strength against yielding

$$P_n = \frac{A_g \times f_y}{\gamma_{mo}} = \frac{1350 \times 250}{1} = 337.5 \text{ kN} > 225 \text{ kN. ....OK}$$

Strength against rupture

As per BS 5950-1:2000 the strength due to or strength against rupture is given by,

$$T_{dn} = \frac{\alpha \cdot A_n \cdot f_u}{\gamma_{m1}}$$

Where,  $\alpha = 0.8$  because number of bolts are 5

Net area = total gross area – area of hole

$$A_n = 1350 - (22 \times 8) = 1174 \text{ mm}^2$$

$$T_{dn} = \frac{0.8 \times 1174 \times 410}{1.25} = 308.05 \text{ kN} > 225 \text{ kN}$$

Strength against block shear

$$p_t = 0.6 \cdot P_y \times t [L_v + k_e (L_t - k \cdot D_t)]$$

Where, Design Strength =  $P_y = 275 \text{ N/mm}^2$

Thickness of section =  $t = 8 \text{ mm}$

Length of member =  $L_v = 280 \text{ mm}$  and  $L_t = 49.5 \text{ mm}$

Eff.Area coeff. =  $K_e = 1.2$

Constant =  $K = 0.5$  and Dia. Of hole =  $D_t = 22 \text{ mm}$

Therefore,  $p_t = 0.6 \times 275 \times 8 [280 + 1.2 (49.5 - 0.5 \times 22)] = 430.05 > 225 \text{ kN}$ .

All checks are satisfied hence the designed member is safe.

### III. PERFORMANCE ANALYSES

The parameters considered for the comparative study of tension member are yield strength, rupture strength and strength due to block shear. The results came from above system development, for these parameters by the design of tension member with IS 800: 2007, AISC 13<sup>th</sup> manual and BS 5950-1:2000 are presented in the table format as below:

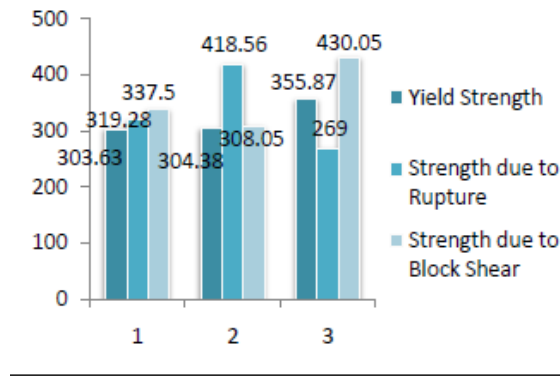
Table 3.1: Parameters for Tension Member

Std. Code	Section Size	Yielding St.	Rupture St.	Shear St.
IS	100×75×8 mm	303.63 kN	304.38 kN	355.87 kN
AISC	L 4 × 3 × $\frac{5}{16}$	71.75 kip	94.06 kip	60.45 kip
		319.28 kN	418.56 kN	269.00 kN
BS : 5950	100×75×8 mm	337.50 kN	308.05 kN	430.05 kN

### IV. RESULT DISSCUSOIN

The values of strengths are different for the same section by the three codes are as given in table no 3.1. for this study, the section sizes may be same or may not be same because of unavailability of same size section in all the three codes, still, tried to keep the sizes of section are near about same. The yield strength of given section by BS code is greater than remaining two codes because of the value of constant used in the formula is greater than other two. Similarly the strength due to rupture by AISC is greater than the IS and BS code. And strength due to block shear is more by BS method as compare to the IS and AISC code. The graphical representation is also express here as follows by using excel.





Graph 4.1

Graph 4.1

## V. CONCLUSION

As per the result discussion it has been observed that, there is variation in the values of the strengths obtained by three different codes because of the variation in the values of the constants considered by the particular code are different and the main thing is that there is unavailability of same size section in all three codes.

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