

Design of Slit Loaded Planar and Curved Patch Antenna



Sumanta Kumar Kundu, Pramod Kumar Singhal

Abstract: Slit loaded circularly polarized patch antenna embedded on planar structure and curvature structure were investigated. The curvature effect on slit loaded patch antenna determines the limiting value of radius of curvature to obtain circular polarization. At a certain radius of curvature (ROC) around 131.3 mm, circular polarization have been obtained with axial ratio band width around 15 MHz and return loss bandwidth around 56 MHz compared with 17 MHz and 65 MHz as that of planar structure. The beam width responsible for coverage of planar patch are 104 and 107 degree with respect to 84 degree and 124 degree of curved patch at $\phi = 0$ and 90 degree respectively.

Keywords : Circular polarization, Curved antenna, Radius of curvature, 3 dB axial ratio beam width

rotation of circular polarized wave will be changed as per feed position in the other diagonal.

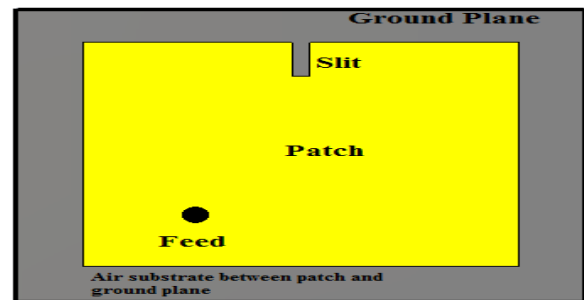


Fig.1: Planar patch

I. INTRODUCTION

Microstrip patch antenna is very much useful and mostly suitable antenna in the category of PCB Technology. The L band communication system is suitable to adopt for mixed communication eg fixed and mobile networks. The base station could use this L band (1-2 GHz as given by IEEE-ITU) for amateur radio service and digital broadcasting services [1-3]. A survey using simulation on embedded curved structured patch antenna is done to find out the limiting value of radius of curvature (ROC) at which this curved structures behaves as planar antenna and almost gives the same result as of planar [4-13]. Curved structure determines the antenna performance. All the simulated work is performed in CST microwave studio [14]. The slit loaded planar patch is designed for circular polarization and the same concept has been applied to achieve circular polarization in curved structure [8-9].

II. DESIGN OF SLIT LOADED PLANAR PATCH

With a square patch of slightly different dimension with one narrow slit having the dimension of width 3.21 mm and length of 12 mm at the centre of one edge is etched for circular polarization [4,7-8]. As indicated in the fig.1 (a), the dimension of square patch is 80.26 mm X 79.63 mm with the thickness of 3.73 mm of air substrate at a designed frequency of 1.65 GHz. The feed point location 8.64 mm from the centre along the one diagonal [4]. The sense of

Due to slit in the centre along the upper edge, the TM_{10} mode have surface current more larger than TM_{01} mode in other direction and creates 90 degree phase shift, which produces CP polarized wave [10]. As given in [7-9], to obtain CP radiation, the slit is adjusted to 3.21 mm X 12 mm. The simulated axial ratio bandwidth and return loss bandwidth are seen to be 17 MHz and 63 MHz at operating frequency of 1.65 GHz indicated in fig 2. Directive -gain in YZ and XZ plane is around 9 dBi with beam width under 3 dB axial ratio at XZ and YZ plane degree are 107 degree 1nd 104 degree respectively and can be calculated from fig 3 (a) and (b).

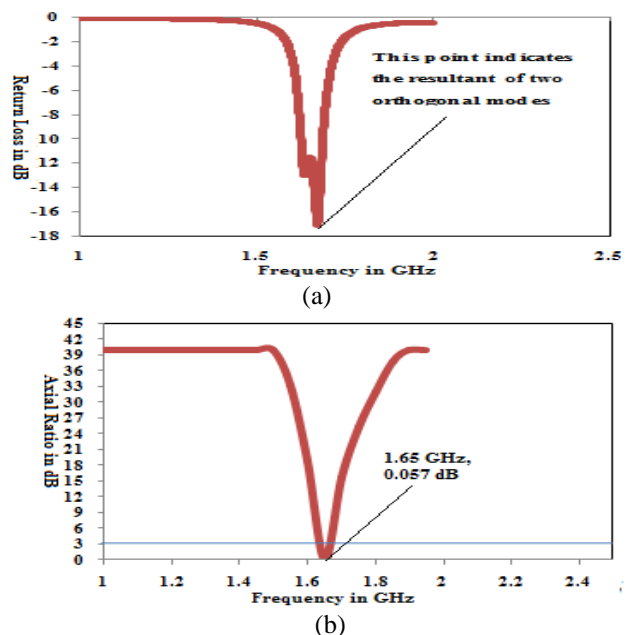


Fig 2 (a) 3 dB AR and (b) S_{11} of diagonally fed and slit loaded planar patch antenna at 1.65 GHz

Revised Manuscript Received on August 14, 2019

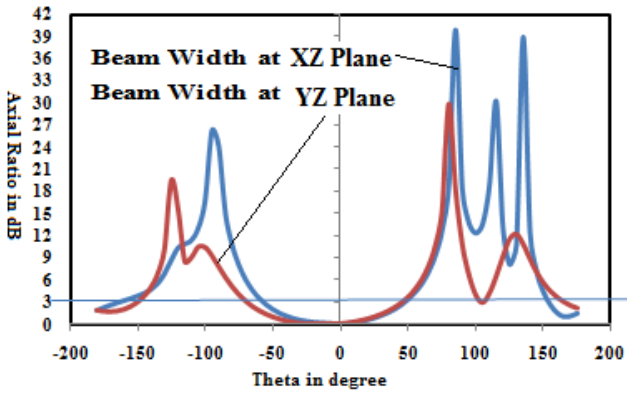
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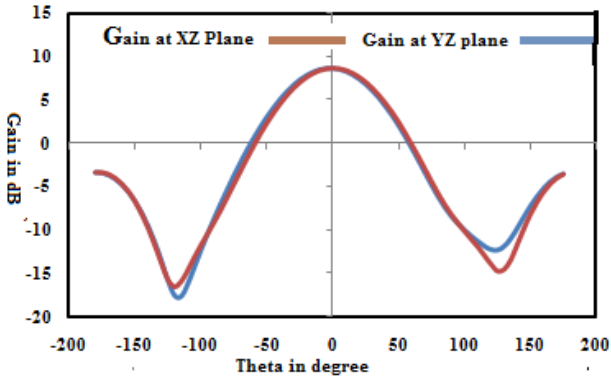
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(a)



(b)

Fig 3 (a) Beam width and (b) IEEE gain of diagonally fed slit loaded planar patch antenna at 1.65 GHz at (a) XZ plane and (b) YZ plane

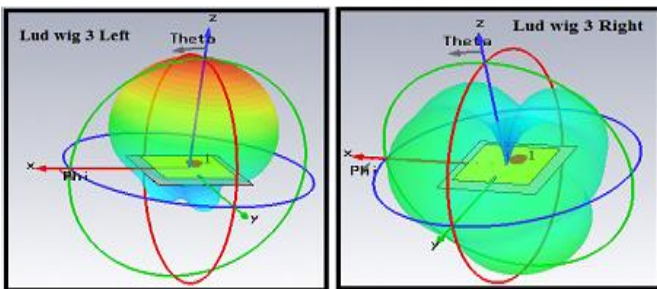


Fig 4 : (a) LHCP radiation (b) RHCP radiation of diagonally fed planar patch antenna at 1.65 GHz

The fig 4.(a-b) indicates the LHCP and RHCP pattern of CP planar patch. Hence LHCP dominates over RHCP as shown in above figure.

III. SLIT LOADED CURVED PATCH

Patch and slit of same dimension as of planar antenna, is embedded on curved surface of having ground plane and air substrate of 3.73 mm height and dielectric constant is 1.00059 as shown in fig 5. The feed point location 8.64 mm from the centre along the one diagonal [4,10].

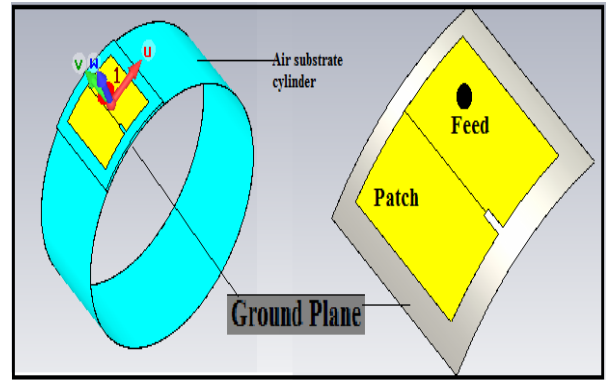
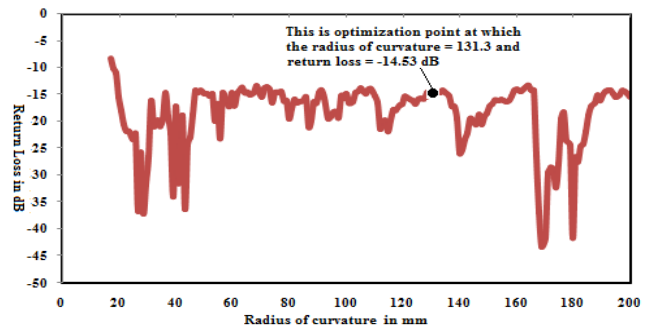
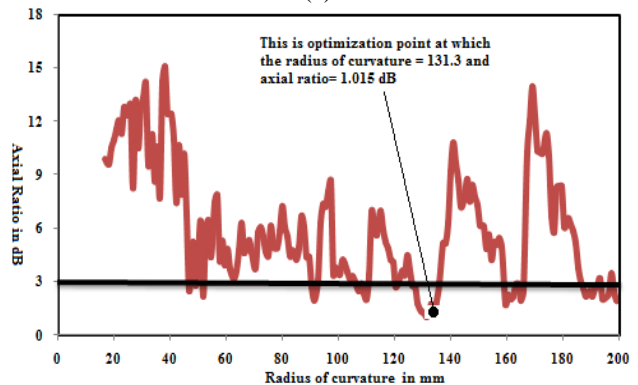


Fig 5: Curved patch design on air substrate designed at 1.65 GHz

The sense of rotation of circular polarized wave will be changed as per feed position in the other diagonal. Due to slit in the centre along the upper edge the TM_{10} mode has surface current more larger than TM_{01} mode in other direction and creates 90 degree phase shift, which produces circular polarized wave [7-8,10]. But the main constraints lie in obtaining circular polarization in curved patch. For that, the radius of curvature is done with the variations of axial ratio and return loss as shown in the fig 6 (a-b). The return loss variation (in fig. 6b) with radius of curvature is found to be very much zigzag because of improper impedance matching of curved surface whereas the variation of axial ratio dictates the improper orthogonality between the two modes TM_{10} and TM_{01} at different radius of curvature



(a)

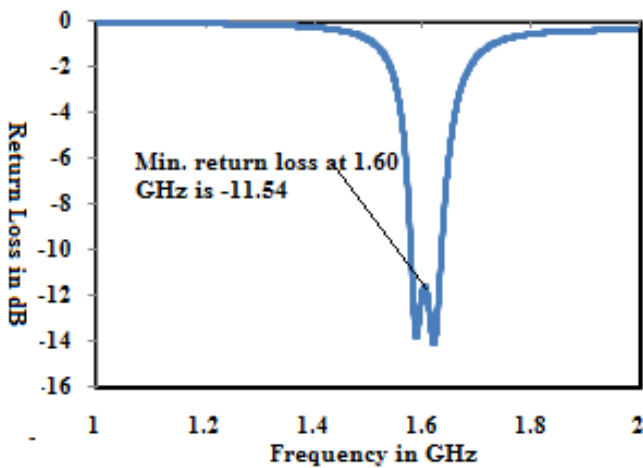


(b)

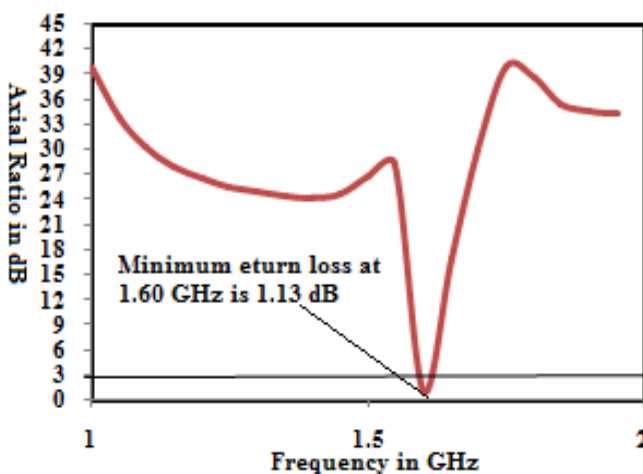
Fig 6. (a) Return Loss (b) Axial ratio with the variation of radius of curvature

The optimized point for radius of curvature for both the result is decided to be $R = 131.30$ mm and accordingly the following results have been obtained for the patch antenna embedded on curved surface as indicated in fig 7 (a-d).

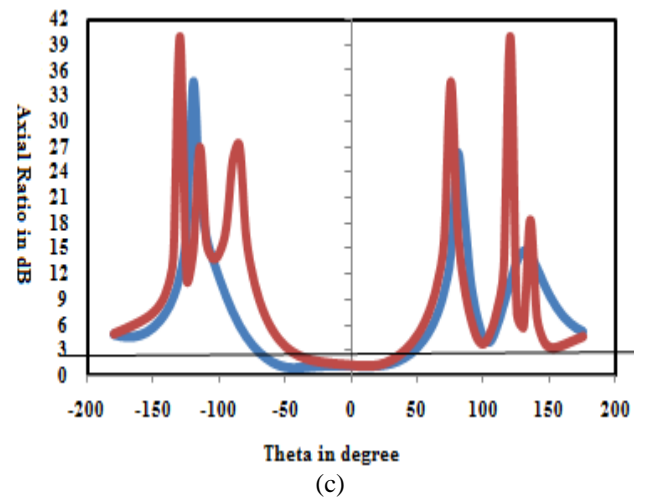
The simulated axial ratio bandwidth and return loss bandwidth are seen to be 15 MHz and 56 MHz as observed in fig 7 (a-b). The patch is resonating for 1.60 GHz in place of 1.65 GHz. In planar antenna both the orthogonal modes were resonating at 1.65 GHz of frequency but when the ground plane and patch bend, due to a large number of basis element function [10-13] and the edge effect due to bending will increase the effective length of the patch [10-13] and frequency decreases to 1.60 GHz. There is another reason for decrease in frequency is slit loading. The slit in the curved patch also bends with the curvature, therefore a single slit can be thought of infinite number tiny slit which increases the total effective length of the patch and hence frequency decreases to 1.60 GHz [10-13]. The result in fig 7 (c) and (d) shows that the coverage angle in XZ plane is 82 degrees and YZ plane is 124 degrees and the gain in XZ and YZ plane seems to be 8.58 dBi. As seen in the fig 7, the resonant frequency for slot loaded curved patch decreases due to curvature effect.



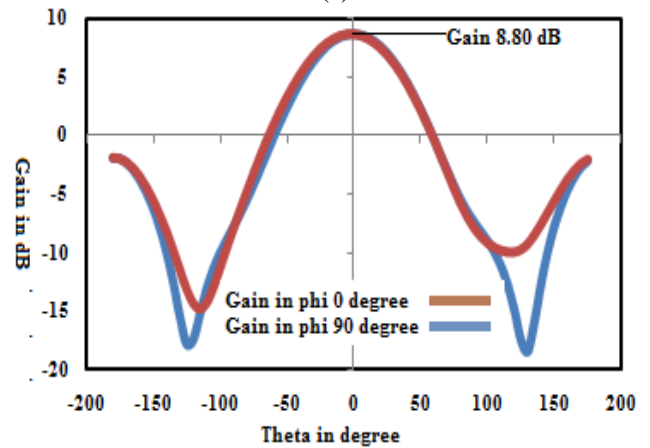
(a)



(b)



(c)



(d)

Fig 7 (a) S_{11} and (b) 3 dB AR (c) 3 dB AR beam width at XZ and YZ plane and (d) IEEE gain of diagonally fed slot loaded cylindrical antenna at 1.60 GHz at $\phi = 0$ degree and $\phi = 90$ degree (all result are taken at radius of curvature = 131.25 mm)

The fig 8 (a) and (b) shows the LHCP and RHCP radiation pattern of CP planar patch. The LHCP is dominated over RHCP in the figure 8.

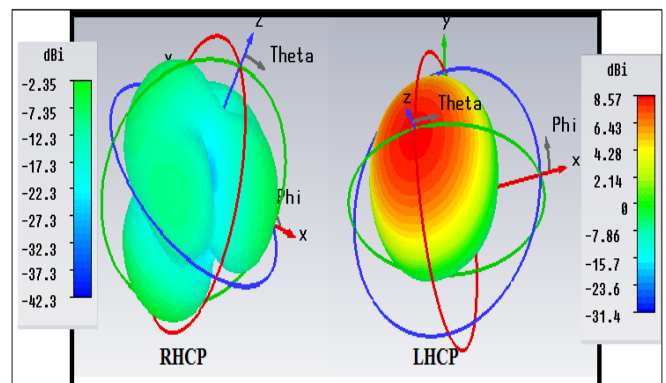


Fig 8 : (a) LHCP radiation (b) RHCP radiation of diagonally fed planar patch antenna at 1.60 GHz

IV. CONCLUSION

A circularly polarized slit loaded patch antenna on planar and curved surfaces has been designed and simulated. The variations of AR and S_{11} with curvature have been studied. The slit loaded curved structure achieves 56 MHz impedance & 17 MHz AR bandwidth. The 3 dB axial ratio beam width obtained at 1.60 GHz is around 84 and 124 degree in XZ and YZ plane. Hence the angular scanning coverage of this patch antenna on curve surface is comparable to planar antenna.

ACKNOWLEDGEMENTS

This work would not have been completed without the software support and encouragement of department of Electronics Engg in Madhav Institute of technology and Science, Gwalior, MP, India.

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